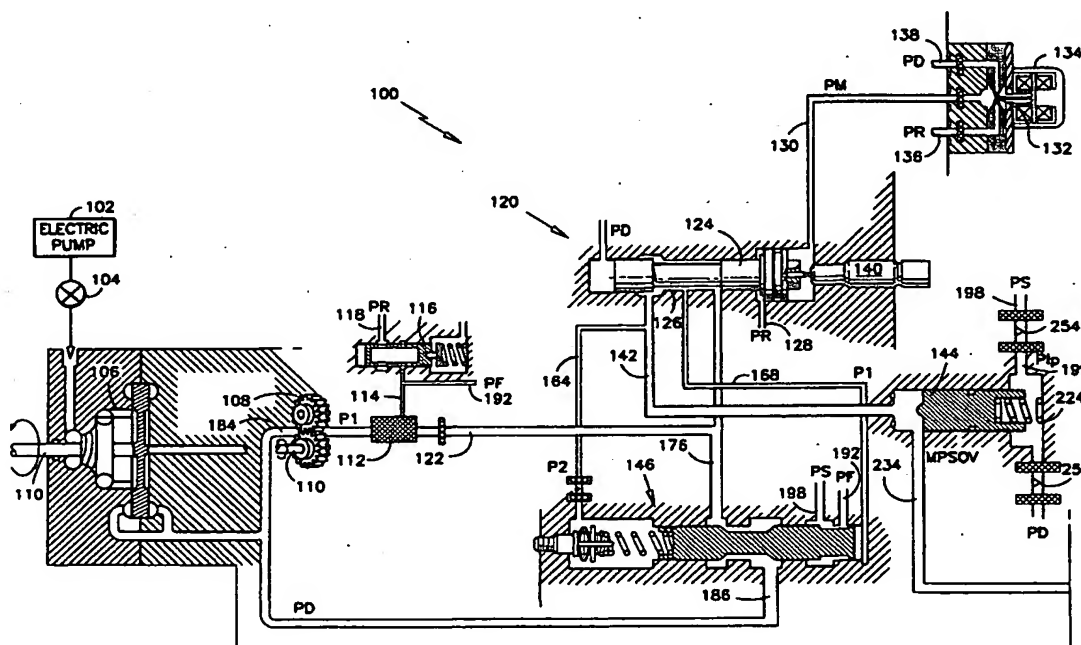




## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

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<p>(21) International Application Number: <b>PCT/US98/26897</b></p> <p>(22) International Filing Date: <b>18 December 1998 (18.12.98)</b></p> <p>(30) Priority Data: 09/004,556      8 January 1998 (08.01.98)      US</p> <p>(71) Applicant: <b>UNITED TECHNOLOGIES CORPORATION</b> [US/US]; Hamilton Standard Division, One Hamilton Road, Windsor Locks, CT 06096-1010 (US).</p> <p>(72) Inventors: <b>DYER, Gerald, P.</b>; 53 Kimberly Drive, Enfield, CT 06082 (US). <b>LENIHAN, Timothy, P.</b>; 9 Brianwood Lane, Granby, CT 06035 (US).</p> <p>(74) Agent: <b>KELLY, Robert, H.</b>; Intellectual Property Counsel, Hamilton Standard, One Hamilton Road, Windsor Locks, CT 06096-1010 (US).</p>		<p>(81) Designated States: JP, European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).</p> <p><b>Published</b> <i>With international search report.</i> <i>Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i></p>

## (54) Title: BI-LEVEL HYDRAULIC PRESSURIZING SYSTEM



## (57) Abstract

A fuel system having a pump (108) for providing a flow of fuel and a metering valve (120) receiving the flow of fuel and providing a regulated flow of fuel consists of a bi-level hydraulic pressurizing system for controlling the output pressure of a fuel supply which includes a pressure regulating valve (146) for maintaining a constant pressure differential across the metering valve. The pressure regulating valve also controls a pressure signal to a pressurization valve (144).

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## Description

BI-LEVEL HYDRAULIC PRESSURIZING  
SYSTEM

## Technical Field

- 5 This invention relates to the control of hydraulic fluid and more particularly to fuel delivery systems for aircraft gas turbine systems.

## Background Art

- It is well known in the art of fuel delivery systems for aircraft gas turbine engines to use a fixed positive displacement pump, such as a vane  
10 or gear pump, to pressurize fuel for subsequent delivery to the engine. The fixed positive displacement pump provides a flow whose volume is a function of the speed at which the pump is rotating. The relation of the change in volumetric output for a change in speed is linear in nature.

- The demand for fuel increases as the speed of the turbine increases,  
15 although when measured as a function of the percentage of pump output, demand for fuel is greatest at either low speeds (engine start) or at high speeds (take-off). Therefore, in order to provide the desired flow of fuel to the turbine during normal flight operation, the excess fuel output from the fixed positive displacement pump must be bypassed from the fuel control  
20 back to the input of the fixed positive displacement pump or to a fuel reservoir.

- The positive displacement pump must be sized to ensure an excess flow capacity at all possible operating conditions. Therefore, the pump must be sized for either low speed start conditions, or high speed takeoff  
25 conditions.

The speed for greatest fuel demand is unique to each engine and is a function of the minimum starting speed. For engine applications where the

pump has been sized, based on start speed, there will be an excess amount of fuel available at higher speeds.

Today's aircraft manufacturers are moving toward lower engine starting speeds, which tend to drive pump design requirements. As  
5 discussed above, sizing pumps for low speed condition generally results in large amounts of bypassed (unused) fuel at higher speed engine operating conditions. This bypassed fuel is continually recirculated and results in significant fuel heating.

With the latest fuel efficient engine designs, excessive fuel heating  
10 becomes a serious problem. The increase fuel temperature requires the addition of fuel/oil coolers. Air is also used to reduce fluid temperatures. These devices increase the cost, weight, and fuel burn of the engine.

It is typical in fuel supply systems for aircraft to control the flow of fuel to the engine through the use of a metering valve in conjunction with a  
15 pressure regulating valve.

Operation of the metering valve and the pressure regulating valve is based upon incompressible flow theory which states that flow through a valve is a function of the area of the valve opening multiplied by the square root of the product of the pressure drop across the valve multiplied by the  
20 specific gravity of the fluid. The pressure regulating valve controls pressure drop across the metering valve and compensates for temperature variations in the fuel, and therefore the flow through the metering valve can be precisely controlled by varying the area of the opening of the metering valve window.

25 In operation, for a desired increase in engine speed, an electronic controller will position the metering valve for a desired flow of fuel to the engine. The speed of the engine will then increase which in turn drives the positive displacement pump at an increased speed. The increase in pump speed will increase the flow of fuel which will cause a rise in the pressure  
30 differential across the metering valve. The pressure regulating valve will then bypass a portion of the fuel output from the positive displacement

pump to maintain the desired pressure differential across the metering valve.

5 In addition to the fuel required by the engine, the pump also provides a fuel flow having a minimum pressure which is a function of the fuel delivery system hardware. The pressurized fuel is used as a working fluid to position valves within the fuel control. Therefore, the fuel must be maintained at sufficient pressure to position the valves and furthermore must have sufficient pressure to actuate the valves within a required response time (slew rate).

10 To maintain the engine fuel at a minimum system pressure, a minimum pressurizing valve is positioned downstream of the fuel metering valve in the engine fuel supply path. The minimum pressurizing valve receives the engine fuel flow as an input and is mechanically biased to close at the desired minimum pressure. Therefore, the pressure of the  
15 engine fuel flow must be greater than the desired minimum pressure in order to force the minimum pressurizing valve open thus allowing the flow of fuel to the engine.

Higher system pressures increase internal leakage of fuel system components and reduce the volumetric efficiency of the pump thus also  
20 increasing pump size.

#### Disclosure of Invention

An object of the present invention is to reduce the minimum required pump size for starting a turbine engine by reducing the system pressure level during engine start to thereby increase the volumetric efficiency of the  
25 fuel pump.

A further object of the present invention is to reduce the minimum required pump size for starting a turbine engine by reducing internal leakage of fuel system components by reducing the system operating pressure during engine start.

A further object of the present invention is to reduce fuel heating by reducing the amount of fuel bypassed during flight mode by minimizing the pump displacement required for proper engine operation.

According to the present invention a fuel delivery system comprises  
5 bi-level hydraulic pressure setting valve which maintains the engine fuel pressure at one of two pressures settings. A first pressure setting (start pressure) is maintained during engine start and a second pressure setting (normal pressure) is maintained for all other engine modes, when operating on the minimum pressurizing valve.

10 The start pressure is determined by the minimum pressure required to provide adequate force margins for valves in the fuel control. This is the minimum pressure required to position the valves in the fuel control for engine start.

The normal pressure is determined by the minimum pressure  
15 required to provide proper performance (i.e. slew rate or transfer times) of valves within the fuel control.

In a fuel delivery system having a fuel pump for pressurizing fuel and a metering valve for regulating the amount of fuel delivered to an engine a bi-level hydraulic pressure setting valve preferably comprises a pressure  
20 regulating valve and associated orifices and a minimum pressurizing valve. The pressure regulating valve controls the pressure differential across the fuel metering valve and controls the input of a pressure signal to the backside of the minimum pressurizing valve. The minimum pressurizing valve ensures that the minimum fuel system pressure level is maintained.

25 Fuel is supplied to the metering valve by a fixed displacement pump whose output increases with pump speed. The pressure regulating valve controls the pressure drop across the metering valve to a desired value by bypassing fuel from the metering valve input to the fixed displacement pump input. Prior to engine start, or lightoff, the pressure regulating valve is  
30 closed such that no fuel is bypassed and the minimum pressurizing valve is initially biased closed by a spring.

During the engine start, fuel pressure builds and the minimum pressurizing valve opens allowing fuel to flow to the engine. The spring is selected such that the minimum pressurizing valve will open when the fuel pressure is sufficient to overcome the force margins necessary to activate the valves within the fuel control allowing the valves within the fuel control to be positioned for engine start.

As the flow and pressure of the fuel increase, the pressure regulating valve will begin to bypass fuel. This bypassing and associated valve movement opens the pressure signal port to the backside of the minimum pressurizing valve. The pressure signal and associated orifices control the increase in the minimum pressure level between start and normal operation.

A first orifice is located upstream of the minimum pressurizing valve and a second orifice is located downstream of the minimum pressurizing valve. The pressure regulating valve, when bypassing, supplies a pressure/flow source which flows through these orifices resulting in an increase in the minimum pressurizing valve opening pressure. The increase in the minimum pressurizing valve opening pressure causes the fuel system pressure to increase to the minimum level required for proper operating performance of the fuel control valves.

The present invention has the utility of reducing the minimum required pump size for starting a turbine engine by reducing the system pressure setting during engine start.

The present invention also has the utility of increasing the volumetric efficiency of the fuel pump by reducing the operating pressure of the pump upon engine start.

The present invention also has the utility of reducing internal leakage of fuel system components by reducing the system operating pressure at engine start.

The present invention also has the utility of reducing fuel heating by reducing the amount of fuel bypassed during flight mode by reducing the pump requirements for engine startup.

### Brief Description of Drawings

FIG. 1 is a schematic view of a fuel delivery system in accordance with the present invention;

FIG. 2 is a cross-sectional view of the pressure regulating/pressure setting valve with pressure setting function during engine start;

FIG. 3 is a cross-sectional view of the pressure regulating/pressure setting valve with pressure setting function during normal engine operation;

FIG. 4 is a cross-sectional view of the minimum pressurizing valve prior to engine start;

FIG. 5 is a cross-sectional view of the minimum pressurizing valve during normal operation.

### Best Mode for Carrying Out the Invention

Referring to FIG. 1, there illustrated is a fuel delivery system 100, preferably for an aircraft engine, according to the present invention. Upon startup or lightoff an electric pump 102 supplies fuel through a solenoid valve 104 to an inducer/boost pump 106 which in turn supplies fuel to the inlet of the positive displacement pump 108. The solenoid valve 104 and electric pump 102 are controlled by the aircraft pilot.

The positive displacement pump 108, is driven by a shaft 110 which in turn is driven by the engine (not shown). Therefore, the amount of fuel delivered by pump 108 is a function of engine speed.

The output of the positive displacement pump 108 is input to a fine screen filter 112 which filters out impurities from the fuel. A portion of the filtered fuel (PF) is delivered through line 114 to a servo pressure regulator 116. The servo pressure regulator produces regulated pressure (PR) on line 118 used for positioning the metering valve 120. PR is at a higher pressure than the pump interstage pressure (PD) which is the pressure at the inlet 184 of positive displacement pump 108. PR and PF are two of the



pressure sources used to position valves within the fuel delivery system  
**100.**

- The majority of the fuel is delivered via fuel line **122** to either the metering valve **120** or the pressure regulating/pressure setting valve (PRV) **146**. The metering valve controls the flow of fuel to the engine by positioning spool **124** which in turn controls the area of the metering valve window **126**.

- The position of the spool **124** is maintained by two counter balancing pressures, PR on line **128**, and the modulated pressure (PM) input on line **130**. The PM on line **130** is controlled by a flapper valve **132** which is positioned by a torque motor **134** in response to a signal from the electronic engine control (EEC not shown). PM is proportional to PR on line **136** and PD on line **138**.

- The EEC determines the desired metering valve **120** position based on the commanded engine speed. Feedback on the position of spool **124** position is provided by an LVDT **140** which is monitored by the EEC. The output of the metering valve **120** is delivered to the minimum pressurizing valve **144** on line **142**. The minimum pressurizing valve **144** sets the inlet pressure of the fuel to be delivered to the fuel control from the positive displacement pump **108**. The function of the minimum pressurizing valve **144** will be described in greater detail herein.

- The flow through the metering valve is proportional to the area of the metering valve window **126** multiplied by the square root of the product of the pressure differential across the metering valve window **126** and the specific gravity of the fuel. Therefore, in order for the metering valve **120** to precisely control the flow of fuel to the engine by varying the area of the metering window **126** the pressure drop across the metering valve **120** must be held at a constant set point. The pressure drop across the metering valve **120** is controlled by the pressure regulating pressure setting valve (PRV) **146**.

The PRV 146 is shown in greater detail in FIG. 2. The PRV 146 consists of a housing 148 having a first end 150 and second end 152 and having a cavity 154 disposed through its length. Slidably located within the cavity 154 is a spool 156 having a low pressure end 158 and high pressure end 160.

Located at the first end 150 of the housing 148 is a port 162 for sensing the metered pressure (P2) of the metered flow on line 164. Located at a second end 152 of the housing is a second port 166 for sensing pressure (P1) of the positive displacement pump output flow on line 168.

10 The positive displacement pump output pressure (P1) acts upon the high pressure end 160 of spool 156. The pressure differential across metering valve 120 is equal to the difference between P1 and P2.

Spring 170 is located within cavity 154 acting upon first end 158 of spool 156. The spring 170 sets the pressure differential to be maintained across the metering valve 120. The spring 170 has sufficient force to hold the spool 156 in a closed position, upon startup or lightoff of the engine as shown in FIG. 2. Adjustment screw 175 allows for manual adjustment of the differential pressure to be maintained across the metering valve 120. The spring 170 is located relative to the housing by spring seat 172.

20 Bi-metallic discs 173 act upon the spring seat 172. The bi-metallic discs 173 expand as the temperature of the fuel increases thus increasing the pressure differential setting across the metering valve. This expansion is needed for this temperature change because the flow through the metering window 126 of valve 120 is proportional to the area of the metering window 126 multiplied by the square root of the product of the pressure drop across the metering window 126 multiplied by the specific gravity of the fuel.

25 The specific gravity of the fuel decreases as the temperature of the fuel increases. Therefore, the pressure differential must be increased for decreases in specific gravity in order to have the expected fuel flow for a given metering window 126 area.

30

There are four ports located along the length of the housing 148 in fluid communication with the cavity 154. The first port 174 receives flow from the output of the positive displacement pump 108 along line 176 and is connected to cavity 154 through first window 180. The second port 182 is an output for providing bypass flow to the inlet 184 of the positive displacement pump 108 along line 186 and is connected to cavity 154 through second window 188. The third port 190 is an input for receiving PF along line 192 and is connected to cavity 154 through third window 194. The fourth port 196 is an output for providing pressure signal (PS) on line 198 to the minimum pressurizing valve 144. The fourth port 196 is connected to cavity 154 through fourth window 200.

The spool 156 has a first land 202, a second land 204 and a third land 206. A first recess 208 separates the first 202 and second 204 lands, and a second recess 210 separates the second 204 and third 206 lands, with the second land 204 being disposed between the first 202 and third 206 lands.

FIG. 2 also shows the PRV 146 in a first, closed position. In this position the force exerted by P1 through line 168 on the high pressure end 160 of the spool 156 is less than the combined force of the spring 170, bi-metallic discs 173, and P2 exerted on the low pressure end 158 of the spool 156. In this position the first land 202 is disposed between the first window 180 and the second window 188 preventing bypass flow to the pump high pressure inlet 184 through line 186. The second land 204 is positioned between the third window 194 and the fourth window 200 preventing PS flow to the low pressure end 224 of the minimum pressurizing valve 144, as shown in FIG. 4.

As the speed of the positive displacement pump 108 increases, the pressure P1 increases such that it is greater than the combined force of P2, spring 170 and bi-metallic discs 173 causing the spool 156 to transition to the left as shown in FIG. 3. The first land 202 is now positioned such that

first window 180 is now in fluid communication with second window 188 through first recess 208 allowing bypass flow to the pump high pressure inlet 184. As the fuel is bypassed the pressure differential across the metering valve 120 will return to the desired set point and the pressure  
5 acting upon spool 156 will be balanced.

As the spool 156 (FIG. 3) travels toward the left, the second land 204 is positioned such that the third window 194 and fourth window 200 are in fluid communication allowing PS to communicate with the low pressure end 224 of minimum pressurizing valve 144 as shown in FIG. 4.

10 The spool and windows of the PRV 146 may be arranged such that the pressure at which fuel is bypassed and the pressure at which PS is ported to the low pressure end 214 of the minimum pressurizing valve 144 may be the same or different.

As the speed of the positive displacement pump 108 decreases, the  
15 process described in the preceding paragraphs is reversed.

The minimum pressurizing valve 144 is shown in greater detail in FIG. 4. The minimum pressurizing valve 144 shown in the closed position, consists of a housing 214 having a first end 216 and second end 218 and having a cavity 220 disposed through its length. Slidably located within the  
20 cavity 220 is a spool 222 having a low pressure end 224 and high pressure end 226. The spool 222 also has a drilled passage 231 to reduce weight.

Located at the first end 216 of the housing 214 is a spring 228. The spring 228 acts upon the low pressure end 224 of the spool 222. Located at a second end 218 of the housing is a regulated fuel inlet 230 for receiving  
25 the metered flow from the metering valve 120 through line 142. The regulated fuel acts on the high pressure end 226 of the spool 222.

There are two ports located along the length of the housing 214 in fluid communication with the cavity 220. The first port 232 is an output to the engine (not shown) along line 234 and is connected to cavity 220

through first window 236. The second port 244 is an input for receiving Plp through line 199 and is connected to cavity 220 through third window 246.

A first orifice 254 is located between the PS 198 and second port 244 and second orifice 256 is located between the second port 244 and PD which is the same pressure as the positive displacement pump inlet 184. The positive displacement pump 108 outlet pressure is a function of 1) pressure drop across the metering valve 120; 2) minimum pressurizing valve spring 228; 3) minimum pressurizing valve 144 cross sectional area; and 4) the ratio of first orifice 254 and the second orifice 256. The following equation provides a method for calculating the positive displacement pump 108 outlet pressure (P1):

$$P1=(MVDP + Fs/Av)/(1-1/(1+(D2^2/D1^2)^2))$$

Where,

P1 is the positive displacement pump 108 outlet pressure (psid) over drain pressure

MVDP is the metering valve 120 pressure drop (psid)

Fs is the minimum pressurizing valve 144 spring force (lbs)

Av is the minimum pressurizing valve 144 cross-sectional area (in<sup>2</sup>)

D1 is the diameter of the first orifice 254 (in)

D2 is the diameter of the second orifice 256 (in)

As stated previously, PF and PR are derived from the output of the positive displacement pump 108 and are used for positioning valves within the fuel delivery system 100.

In operation, the minimum pressurizing valve 144 acts in concert with the PRV 146 to regulate the pressure of the metered fuel flow to the engine. As discussed in the preceding paragraphs, upon engine start the pressure drop across the metering valve 126 is relatively low therefore the pressure at the high pressure end 160 of the PRV 146 is less than the force exerted by the spring 170 and bi-metallic disc 173 and P2. This causes the spool

156 to be positioned as shown in FIG. 2 preventing PS from flowing to the low pressure end 224 of the minimum pressurizing valve 144.

Therefore, the pressure of the metered fuel needed to force the spool 222 to the open position as shown in FIG. 4 must be greater than the pressure exerted by the spring 228 and Plp thus maintaining the regulated fuel at the pressure as determined by the spring force of the spring 228 and Plp. As discussed, this pressure is selected to be the minimum needed to position the valves in the fuel control for engine start.

As the engine speed increases, the shaft 110 speed increases which increases the output of the fixed displacement pump 108. This in turn increases the pressure differential across the metering valve 126. The pressure P1 at the high pressure end 160 of the PRV 146 is greater than the force exerted by the spring 170 and the bi-metallic disc 173 and P2 on the low pressure end 158 of the PRV 146 causing the spool 156 to translate to the position shown in FIG. 3 allowing PS to flow, through line 198, to the low pressure end 224 of the minimum pressurizing valve 144. Thus, the pressure at the low pressure end 224 is now determined by Plp and spring 228.

Metered fuel flow delivered to the minimum pressurizing valve 144 from the metering valve 120 on line 142 must now have a pressure greater than the combined force of the spring 228 and Plp input through second port 224, thus maintaining the pressure of the metered fuel flow at a higher minimum pressure. This minimum pressure is selected to meet the slew rate requirements of the valves in the fuel control to allow for normal operation of the engine.

It should be understood by those skilled in the art that obvious structural modifications can be made without departing from the spirit of the invention. Accordingly, reference should be made primarily to the accompanying claims, rather than the foregoing specification, to determine the scope of the invention.

The present invention has the utility of reducing the minimum required pump size for starting a turbine engine by reducing the system pressure setting during engine start.

5 The present invention also has the utility of increasing the volumetric efficiency of the fuel pump by reducing the operating pressure of the pump upon engine start.

The present invention also has the utility of reducing internal leakage of fuel system components by reducing the system operating pressure at engine start.

10 The present invention also has the utility of reducing fuel heating by reducing the amount of fuel bypassed during flight mode by reducing the pump requirements for engine startup.

We claim:

## Claims

1. A bi-level hydraulic pressurization system for regulating a pressure of a fluid comprising:
  - a sensing means for sensing a flow rate of the fluid, wherein said sensing means provides a pressure signal when said flow rate of the fluid is greater than a first value; and
  - a pressurizing means for controlling the pressure of the fluid, wherein said pressurizing means is responsive to said pressure signal for controlling the pressure of the fluid to a first minimum pressure when said flow rate is less than said first value and wherein said pressurizing means controls the pressure of the fluid to a second minimum pressure when said flow rate greater than said first value.
2. The bi-level hydraulic pressurization means of Claim 1 wherein said pressurizing means further comprises a biasing means for setting said first and said second minimum pressures.
3. The pressurizing means of Claim 2 wherein said biasing means comprises a spring for setting said first minimum pressure.
4. The pressurizing means of Claim 3 wherein said biasing means further comprises a means for responding to said pressure signal for setting said second minimum pressure.
5. A fuel delivery system for providing a metered fuel flow to an engine, having a pump providing an unregulated fuel flow for positioning valves within the fuel delivery system comprising:



a metering means for providing the metered fuel flow, said metering means in fluid communication with the pump means for receiving said unregulated fuel flow;

a bypass means for regulating the pressure differential across said metering means by regulating a bypass flow of the unregulated fuel from said metering means to the pump;

a sensing means for sensing said bypass flow wherein said sensing means provides a pressure signal when said bypass flow exceeds a value; and

a pressurizing means for setting the output pressure of the metered fuel flow, said pressurizing means responsive to said pressure signal, wherein said pressurizing means sets the output pressure to a first minimum pressure when said bypass flow is less than said value and wherein said pressurizing means sets the output pressure to a second minimum pressure when said bypass flow is greater than said value.

6. The fuel delivery system of Claim 5 wherein said pressurizing means further comprises a biasing means for setting said first and said second minimum pressures.

7. The fuel delivery system of Claim 6 wherein said biasing means comprises a spring for setting said first minimum pressure.

8. The fuel delivery system of Claim 7 wherein said biasing means further comprises a means for responding to said pressure signal for setting said second minimum pressure.

9. The fuel delivery system of Claim 5 wherein said first minimum pressure is equal to a pressure necessary to overcome a force margin of the valves.

10. The fuel delivery system of Claim 5 wherein said second minimum pressure is equal to a pressure necessary to meet a slew rate requirement of the valves.

11. A fuel delivery system for providing a metered fuel flow to an engine, comprising:

a first pump means for providing an unregulated fuel flow;

a metering means for providing the metered fuel flow to the engine, said metering means in fluid communication with said first pump means for receiving said unregulated fuel flow;

a pressure regulation means for setting a pressure differential across said metering means, said pressure regulation means having a means for sensing a bypass flow of unregulated fuel, wherein said pressure regulation means having a means for providing said bypass flow from said metering means to said first pump means for adjusting said pressure differential, and wherein said pressure regulation means providing a pressure signal when said bypass flow is greater than a first value ; and

a pressurizing means for controlling a pressure of the metered fuel flow wherein said pressurization means is responsive to said pressure signal for controlling said pressure of the metered fuel flow to a first minimum pressure when said bypass flow is less than said first value and wherein said pressurizing means controls said pressure of the metered fuel flow to a second minimum pressure when said bypass flow is greater than said first value.

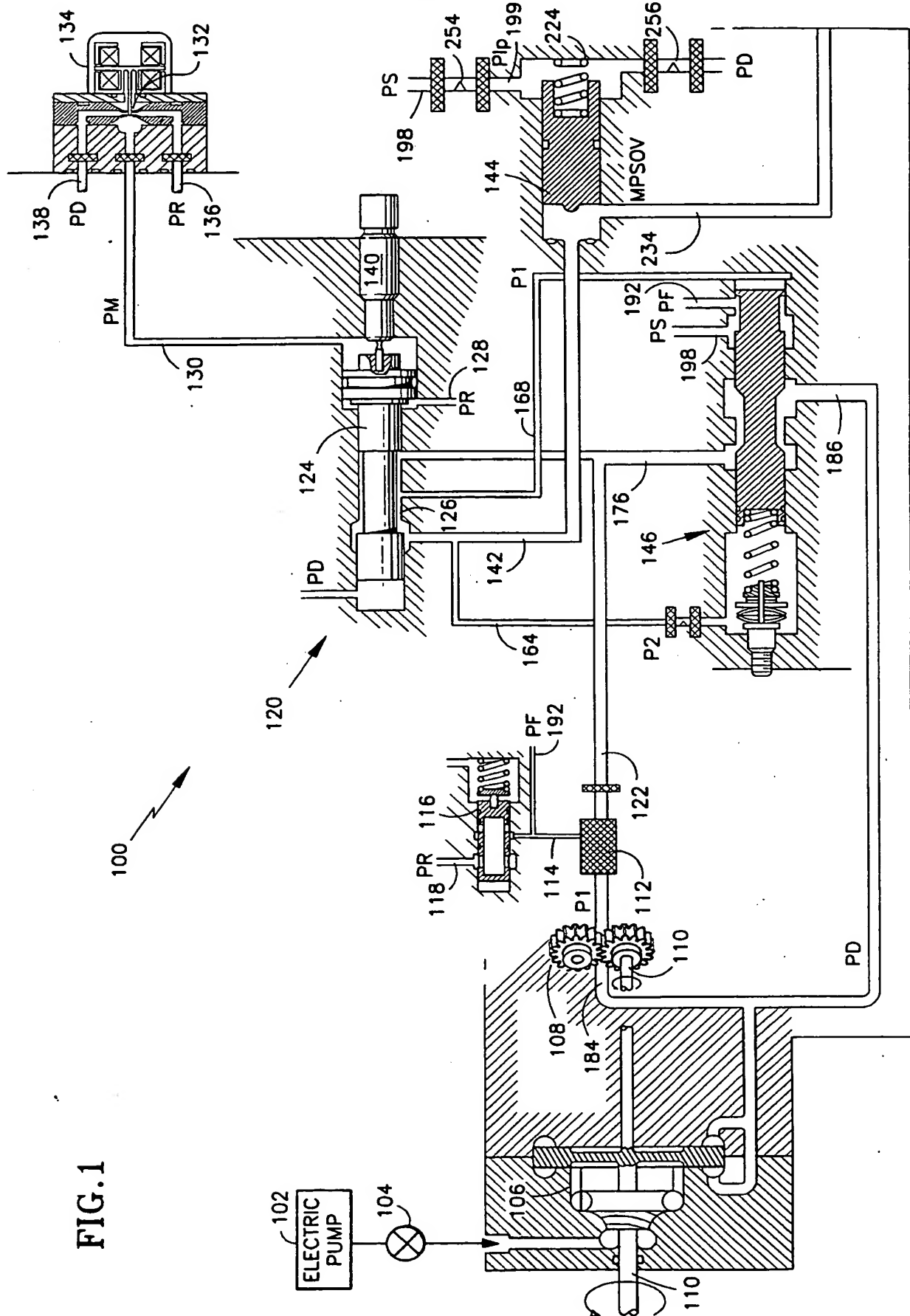
12. The fuel delivery system of Claim 11 further comprising a biasing means for setting said first and said second minimum pressures.

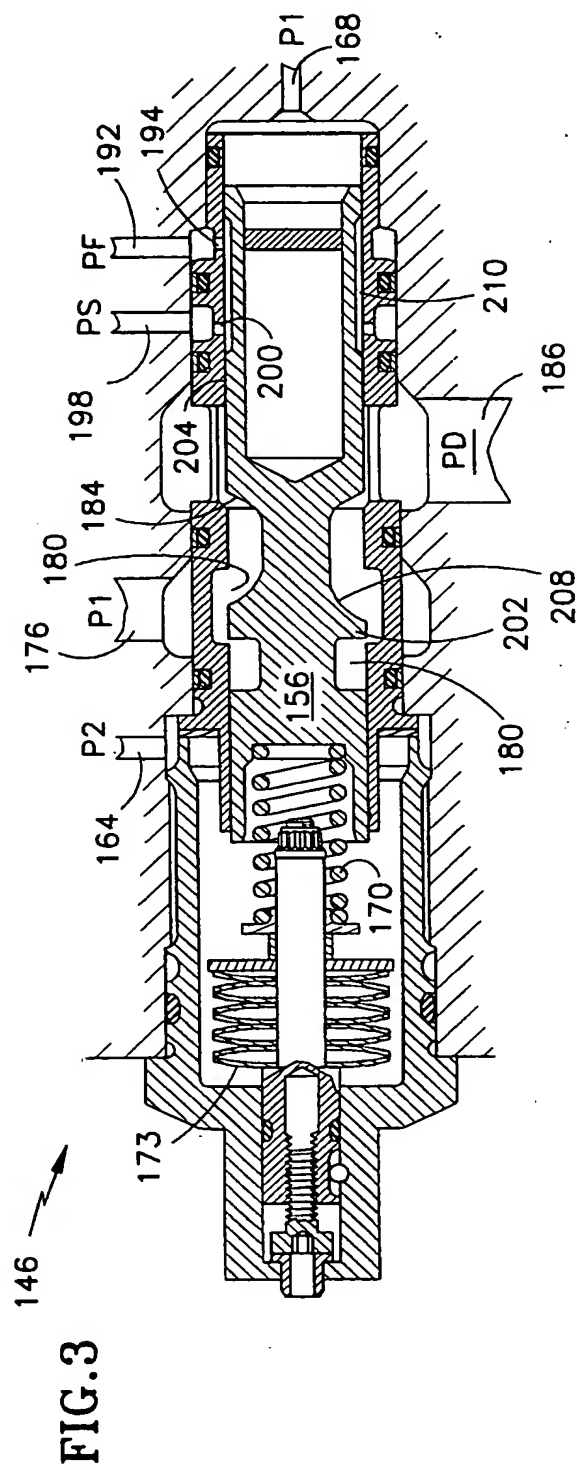
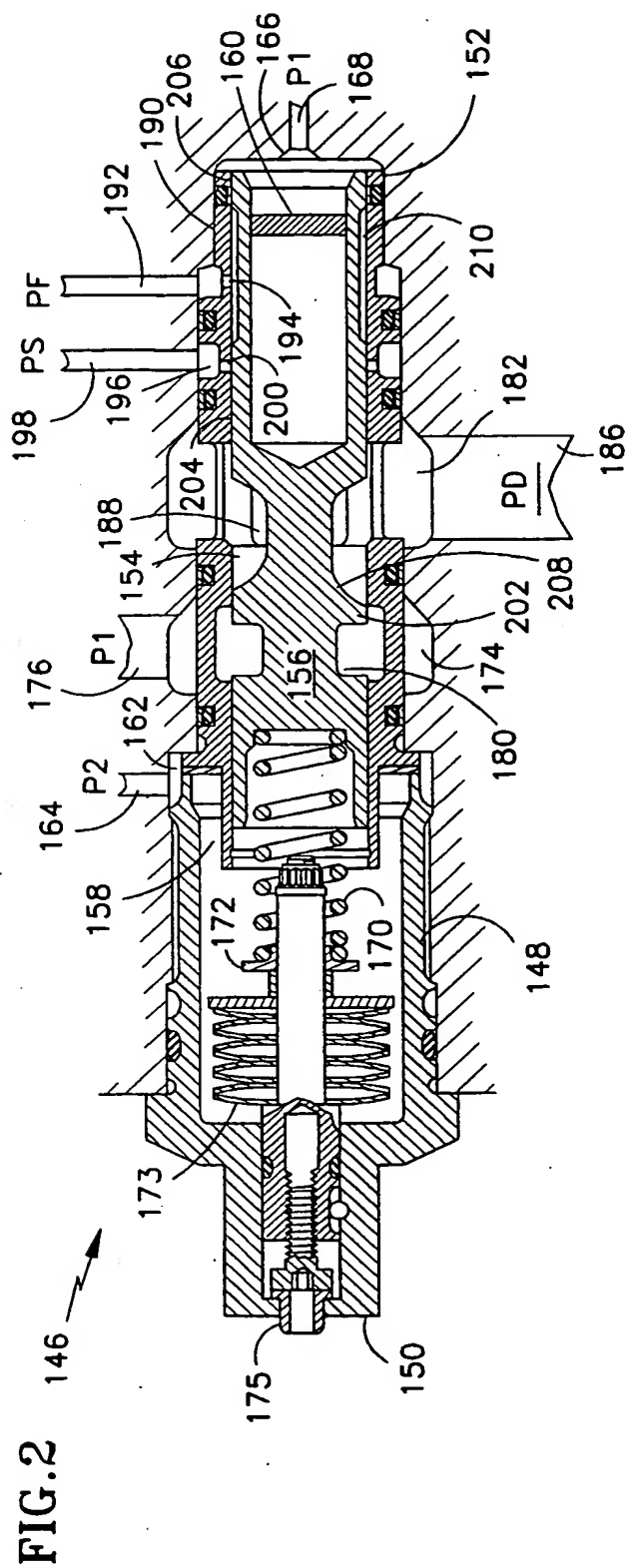
13. The fuel delivery system of Claim 12 wherein said biasing means comprises a spring for setting said first minimum pressure.

14. The fuel delivery system of Claim 13 wherein said biasing means further comprises a means for responding to said pressure signal for setting said second minimum pressure.

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FIG. 1





3/3

FIG.4

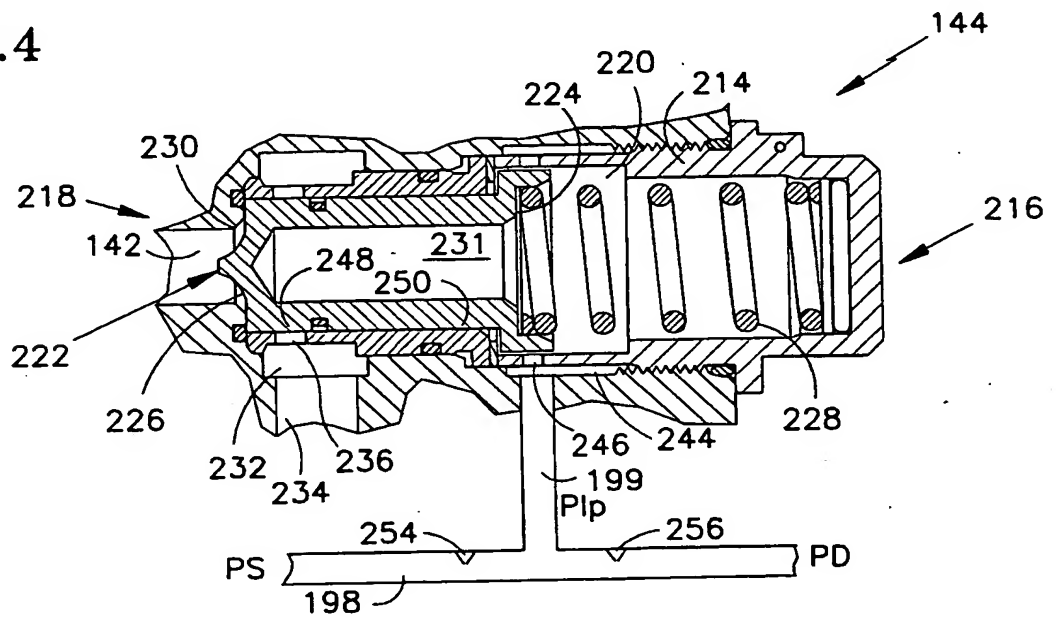
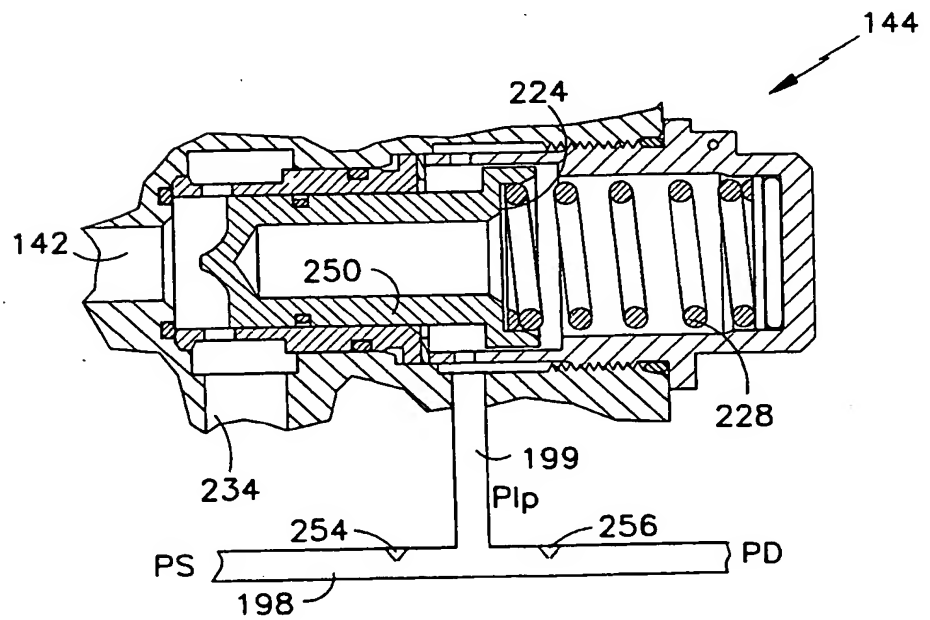


FIG.5



## INTERNATIONAL SEARCH REPORT

International application No.

PCT/US98/26897

## A. CLASSIFICATION OF SUBJECT MATTER

IPC(6) :FO2C 9/26

US CL :60/39.281

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 60/39.281, 734

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 3,808,798 A (TAYLOR) 07 May 1974, see elements 90 and 98.	1-14
Y	US 4,493,187 A (HANSEN) 15 January 1985, see elements 60 and 115.	1-14
Y	US 4,817,376 A (BROCARD et al) 04 April 1989, see element 5.	1-14
Y	US 5,209,058 A (SPARKS et al) 11 May 1993, see elements 70 and 75.	1-14



Further documents are listed in the continuation of Box C



See patent family annex.

*A*	Special categories of cited documents	*I*	later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
*B*	document defining the general state of the art which is not considered to be of particular relevance	*N*	document of particular relevance, the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
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